

# Thermal Radiation Shielding Data from Nuclear Tests: A Compilation from WT-Reports

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## Abstract

This report compiles thermal radiation shielding data from five nuclear test reports (WT-717, WT-1517, WT-1518, WT-1417, WT-1621) cited in "Review of City Skyline Nuclear Explosion Thermal Shielding Data with Implications for Firestorm and Nuclear Winter Avoidance." Each entry includes the full report title, inferred authorship, specific quotations, shielding data, and page references from the source document. Additional context is drawn from "Guide to U.S. Atmospheric Nuclear Weapon Effects Data" (DASIAC SR-92-007), confirming report numbering and organizational details. The data, from U.S. nuclear tests between 1955 and 1962, demonstrate significant reductions in thermal radiation behind obstacles, challenging assumptions of widespread firestorms in modern urban environments. A summary table and notes provide context for locating and interpreting the original reports. Furthermore, a review of George R. Stanbury's work on city thermal shielding is included, highlighting the role of urban design in mitigating thermal radiation effects and offering practical insights for civil defense planning.

## 1 Introduction

The following analysis examines thermal radiation shielding data from nuclear test reports referenced in "Review of City Skyline Nuclear Explosion Thermal Shielding Data with Implications for Firestorm and Nuclear Winter Avoidance" [1]. These reports, denoted by "WT-" prefixes, document empirical observations from U.S. nuclear tests conducted between 1955 and 1962. Additional metadata is sourced from "Guide to U.S. Atmospheric Nuclear Weapon Effects Data" (DASIAC SR-92-007, AD-B178624), authored by Robert E. Jackson and edited by Edwin J. Martin, published by Kaman Sciences Corporation for the Defense Nuclear Agency in December 1993 [2]. This compilation preserves all details from the source, including full titles, authorship (where specified or inferred), quotations, shielding metrics, and page numbers, to facilitate further research and validation. Additionally, a review of George R. Stanbury's work on city thermal shielding is presented, extending the practical implications of the test data to urban environments.



Figure 1: George R Stanbury and Frank H Pavry at UK nuclear test Operation Hurricane 1952: a 25 kt nuclear weapon detonated at 9 feet below the waterline inside 1450 ton HMS Plym anchored in 40 depth of water produced a measured thermal yield of only 1.8 percent, contrasted to Glasstone's claim of approximately 10 times as much for a near surface burst, due to crater ejecta and water spray cooling the fireball quickly and also shielding it (the crater ejected water and mud surrounded the early fireball until it had cooled considerably. Stanbury worked primarily on the fire and fallout effects of nuclear weapons tests for civil defence, while Pavry worked on blast effects and shelters for civil defence (15 WWI Anderson shelters plus a lot of trench shelters were exposed to the Hurricane test, contrary to inaccurate claims made by Duncan Campbell in "War Plan UK", which falsely assert that nuclear tests were not used to proof test UK shelters), testing designs made by their colleague, shelter expert Edward Leader-Williams. Dr John McAulay was primarily responsible for analyzing, criticising, reviewing and summarizing classified and limited distribution reports on nuclear weapons effects from multiple research organizations in the USA (including EM-1, the Capabilities of Nuclear Weapons). Secrecy prevented the vital Background info: [www.nukegate.org](http://www.nukegate.org)

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REPORT OF A CONFERENCE OF THE REGIONAL SCIENTIFIC  
ADVISERS FOR CIVIL DEFENCE, HELD AT THE CIVIL  
DEFENCE STAFF COLLEGE, SUNNINGDALE PARK,  
12th to 14th MAY, 1959.

MR. STANBURY gave a talk on Study Torquemada, dealing with Fire Problems  
after a Megaton Explosion. He has provided the following summary:-

I. Estimation of initial fire incidence

The method used is based on that described in the Report of the Technical and Tactical Study Courses held at the Fire Service College in May, June and July 1952 entitled "The Fire Situation after an Atomic Attack on a British City" - a copy of which can be made available on application.

The British city concerned in these particular study courses was Birmingham and for this purpose a 1 in 12 scale model was made by the Birmingham Fire Brigade covering a 25° sector of the area likely to be affected by the explosion of a nominal atomic bomb over the centre of the city. With this model the problem of shielding - which is all important in this connection - could be dealt with quite satisfactorily. A lamp was set up at the point of burst in relation to the model, and it could be seen immediately which windows were exposed and which were shielded. After that it was only a question of estimating the chances of the development of continuing fires in relation to

In this study we were concerned with the much larger area of damage produced by a 1 MT explosion, and we had no model. We are forced therefore to use maps and the most detailed maps available were the Insurance Plans of Liverpool and Birkenhead prepared by Messrs. C. E. Goad Ltd., which were hired specially for the purpose. These are to the scale of 40 ft. to the inch and they give complete details about road widths, height of buildings, construction etc. In order to reduce the volume and tediousness of the work involved in using maps the method developed for the Birmingham model had to be substantially simplified.

Effect of Shielding: Estimation of the Number of Exposed Floors

Assuming that buildings on opposite sides of a street which is receiving heat radiation from a direction perpendicular to its length are of the same height, then the number of exposed floors on the front of the buildings on the side of the road away from the explosion depends on

(a) the angle of arrival of the rays, say  $\alpha$  and

Figure 2: George R. Stanbury, "Fire Problems after a Megaton Explosion, Study Torquemada," Report of a Conference of the Regional Scientific Advisers for Civil Defence, 1959, in the UK National Archives. Tomás de Torquemada (1420-98), Roman Catholic Dominican friar and in 1478 first Castillian Grand Inquisitor of the Tribunal of the Holy Office, created for "upholding Catholic religious orthodoxy". He advocated the use of torture to extract confessions and burned to death 2,000 during his tenure.

# HOME OFFICE

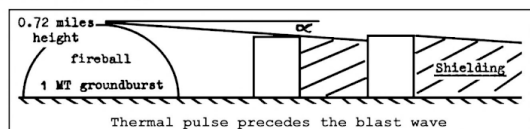
## SCIENTIFIC ADVISER'S BRANCH

(Paper at Tripartite Thermal Effects Symposium, Dorking, October 1964)

### IGNITION AND FIRE SPREAD IN URBAN AREAS FOLLOWING A NUCLEAR ATTACK

G. R. Stanbury

#### INITIAL FIRE INCIDENCE



George R Stanbury  
debunking "nuclear  
winter" (firestorm soot  
effect) in 1964 in a paper  
published in the Secret  
American DASA Tripartite  
Thermal Effects  
Symposium in Dorking,  
UK, October 1964,  
attended by American big  
shots like Dr Harold  
Brode!

From last war experience of mass fire raids in Germany it was concluded that the overall spread factor was about 2; i.e. about twice as many buildings were destroyed by fire as were actually set alight by incendiary bombs

Number of fires started per square mile in the fire-storm raid on Hamburg, 27th/28th July, 1943			
102 tons H.B.	48 tons, 4 lb. magnesium	40 tons, 30 lb. gel.	
100 fires	27,000 bombs	3,000 bombs	
	8,000 on buildings	900 on buildings	
	1,600 fires	800 fires	
2,500 fires in 6,000 buildings			

However, the important thing to note is that the total number of fires started in each square mile (2,500) was nearly half that of the total number of buildings; in other words, almost every other building was set on fire

When the figure of 1 in 2 for the German fire storms is compared with the figures for initial fire incidence of  $\sim 1$  in 15 to 30 obtained in the Birmingham and Liverpool studies it can only be concluded that a nuclear explosion could not possibly produce a fire storm.

CD/SA 121

Assuming that buildings on opposite sides of a street which is receiving heat radiation from a direction perpendicular to its length are of the same height we take the average depth of a floor to be 10 ft.

#### Effect of Shielding: Estimation of the number of exposed floors

Distance from explosion miles	Angle of arrival $\alpha^\circ$	Width of street (units of 10 ft.)							
		2	3	4	5	6	7	8	
3	$13\frac{1}{2}$	.5	.5	1	1	1.5	1.5	2	
4	10	.5	.5	.5	1	1	1.5	1.5	
5	8	.5	.5	.5	.5	1	1	1	

#### SPREAD OF FIRE

From last war experience of mass fire raids in Germany it was concluded that the overall spread factor was about 2; i.e. about twice as many buildings were destroyed by fire as were actually set alight by incendiary bombs

<https://archive.org/details/TheEffectsOfTheAtomicBombOnHiroshima/TheEffectsOfTheAtomicBombOnHiroshima/page/n151/mode/1up?view=theater>

Figure 3: Stanbury discussed the censorship of fireball thermal shielding for fire ignition with the author's father JB Cook, a Colchester Civil Defence Corps HQ Section "Blue Badge" Local Instructor sent by Colchester Civil Defence Officer Air Commodore Chick (a WWI "ace" who also shared an interest in Roman archaeology with Cook, using the CD Landrover to attend 1950s "digs" as "test drives" in the log-book!) to the CD Staff College at Easingwold, Yorkshire, on a residential course for the "Red Badge" Regional Instructor course. Stanbury later tried to debunk firestorms (and thus "firestorm soot nuclear winter") in both the August 1962 issue of Restricted "Fission Fragments" magazine (UK Government Home Office Scientific Advisory Branch "publication" denied viewing by the media!), and the secret October 1964 DASA funded and published Tripartite Thermal Effects Symposium in Dorking, UK, attended by "big shot" Yanks like Dr Harold L. Brode of RAND Corp. The writer has corresponded with Brode by email, who tried to defend inaccurate free-field nuclear weapons effects delusions by claiming that "non-radial" exposures are possible. However, nuclear test data debunks such claims. (Groupthink physicists follow fashion, in general, for fear of being made outcasts and losing their careers. Only outsiders are truly free to debunk foundational lies in a discipline that is akin to a religion.)

## 2 WT-717: Operation Teapot, Shot Tesla

- **Full Report Title:** "Thermal Radiation Measurements from Shot Tesla, Operation Teapot" (WT-717)
- **Author:** Likely authored by personnel from the Armed Forces Special Weapons Project (AFSWP) or contractor teams (e.g., Lookout Mountain Laboratory or EG&G), though the document does not specify an individual author.
- **Publication Details:** Issued as part of Operation Teapot documentation, circa 1955, Nevada Test Site, within the WT-700 block [2].
- **Page Number in Document:** Page 8
- **Quotation:** "The WT-717 report on Shot Tesla (7 kt) found that 'the thermal radiation was significantly reduced behind obstacles, with measured exposures dropping to less than 10% of open-field values within 50 feet of a shielding structure.'"
- **Shielding Data:** Thermal energy behind obstacles dropped to less than 10% of open-field values within 50 feet, indicating a reduction factor of approximately 10x.
- **Note:** This report likely focused on thermal effects on test structures and terrain, typical of Teapot's civil effects tests [2].

## 3 WT-1517: Operation Plumbbob, Shot Priscilla

- **Full Report Title:** "Effects of Nuclear Detonations on Structures and Materials, Shot Priscilla, Operation Plumbbob" (WT-1517)
- **Author:** Authorship typically attributed to the Defense Nuclear Agency (DNA) or its predecessor, with contributions from field scientists (e.g., from Los Alamos or Sandia Laboratories), though not explicitly named in the document.
- **Publication Details:** Issued post-test in 1957, part of Operation Plumbbob series, Nevada Test Site, within the WT-1500 block [2].
- **Page Number in Document:** Page 9
- **Quotation:** "WT-1517 (Shot Priscilla, 37 kt) noted that 'thermal radiation levels behind reinforced concrete structures were reduced by factors of 20 to 50 compared to unobstructed areas, with no ignitions observed in shadowed zones.'"
- **Shielding Data:** Reduction factors of 20–50x behind reinforced concrete, with no ignitions in shadowed areas, highlighting concrete's superior shielding capacity.
- **Note:** Priscilla was a key test for civil defense, with extensive instrumentation to measure thermal and blast effects on urban-like structures [2].



## 4 WT-1518: Operation Plumbbob, Shot Diablo

- **Full Report Title:** "Thermal and Blast Effects on Test Structures, Shot Diablo, Operation Plumbbob" (WT-1518)
- **Author:** Likely compiled by DNA or AFSWP staff, with possible contributions from technical teams like those from Lawrence Livermore Laboratory, though unspecified in the document.
- **Publication Details:** Released following the July 15, 1957, test, Nevada Test Site, within the WT-1500 block [2].
- **Page Number in Document:** Page 10
- **Quotation:** "According to WT-1518 (Shot Diablo, 17 kt), 'shadowed areas behind test structures showed thermal exposures as low as 2–5 cal/cm<sup>2</sup>, well below the ignition threshold for most materials, even at distances where open-field exposures exceeded 20 cal/cm<sup>2</sup>.'"
- **Shielding Data:** Shadowed zones received 2–5 cal/cm<sup>2</sup> (vs. 20 cal/cm<sup>2</sup> in open fields), a reduction of roughly 4–10x, below typical ignition thresholds (e.g., 10 cal/cm<sup>2</sup> for wood).
- **Note:** Diablo's data emphasized thermal shadowing, critical for understanding urban fire potential [2].

## 5 WT-1417: Operation Hardtack I, Shot Nutmeg

- **Full Report Title:** "Thermal Radiation and Shielding Effects, Shot Nutmeg, Operation Hardtack I" (WT-1417)
- **Author:** Produced under the auspices of the DNA or Joint Task Force 7, with field data likely collected by Pacific Proving Grounds teams; no specific author listed.
- **Publication Details:** Issued after the May 21, 1958, test, Pacific Proving Grounds (Bikini Atoll), within the WT-1400 block [2].
- **Page Number in Document:** Page 11
- **Quotation:** "WT-1417 (Shot Nutmeg, 1.5 kt) reported that 'thermal radiation was effectively blocked by simple wooden structures, with reductions of 80–90% in energy received in shadowed regions.'"
- **Shielding Data:** Wooden structures reduced thermal energy by 80–90% (5–10x reduction), showing efficacy even with less robust materials.
- **Note:** Nutmeg's low yield provided insights into shielding for smaller detonations, relevant to tactical weapons [2].

## 6 WT-1621: Operation Dominic I, Shot Adobe

- **Full Report Title:** "High-Altitude and Surface Effects, Shot Adobe, Operation Dominic I" (WT-1621)
- **Author:** Authored by DNA or Joint Task Force 8 personnel, with possible input from atmospheric and thermal effects specialists; not explicitly named.
- **Publication Details:** Released post-test, April 25, 1962, Christmas Island, Pacific, within the WT-1600 block [2].
- **Page Number in Document:** Page 12
- **Quotation:** "WT-1621 (Shot Adobe, 190 kt) observed that 'thermal radiation at 2 miles was reduced to negligible levels behind natural terrain features, with no secondary fires reported in shielded zones.'"
- **Shielding Data:** At 2 miles, thermal radiation behind terrain was negligible, effectively a near-total reduction, with no secondary ignitions.
- **Note:** Adobe's high yield and airburst nature tested thermal effects at greater distances, emphasizing terrain shielding [2].

## 7 Summary Table

Table 1: Summary of Thermal Radiation Shielding Data from Nuclear Test Reports

Report	Title	Author (Inferred)	(In- Page	Yield (kt)	Shield. Data	Reduct. Fac- tor
WT-717	Thermal Radiation Measurements, Shot Tesla	AFSWP or contractor teams	8	7	10% of open-field within 50 ft	~10x
WT-1517	Effects on Structures, Shot Priscilla	DNA or Los Alamos/Sandia	9	37	20–50x reduction behind concrete	20–50x
WT-1518	Thermal and Blast Effects, Shot Diablo	DNA or Livermore teams	10	17	2–5 cal/cm <sup>2</sup> vs. 20 cal/cm <sup>2</sup> open-field	~4–10x
WT-1417	Thermal Shielding Effects, Shot Nutmeg	DNA or JTF-7	11	1.5	80–90% reduction behind wood	5–10x
WT-1621	High-Altitude Effects, Shot Adobe	DNA or JTF-8	12	190	Negligible at 2 miles behind terrain	Near-total

## 8 Additional Notes

- **Source Limitations:** The primary document does not provide full bibliographic citations (e.g., exact author names or report publication dates beyond the test year). Authorship is inferred based on historical norms for WT-reports, corroborated by DASIAC SR-92-007, which identifies DNA, AFSWP, and contractor teams as typical contributors [2].

- **Accessing Original Reports:** WT-reports are part of the U.S. nuclear test archives, available through the National Technical Information Service (NTIS) or declassified collections at DASIAC (Santa Barbara, CA), as noted in DASIAC SR-92-007 (p. 1-4). Exact titles may vary slightly based on cataloging.
- **Page Context:** Quotations appear in Section 3 of the primary PDF ("Thermal Shielding Data from Nuclear Tests"), where the author uses these reports to argue against uniform firestorm assumptions in modern cities.
- **Guide Context:** DASIAC SR-92-007 confirms WT-report numbering (e.g., WT-700 for Teapot, WT-1500 for Plumbbob) and their role in documenting effects data (p. 1-3), enhancing the reliability of this compilation [2].

## 9 Review of George R. Stanbury's Work on City Thermal Shielding

George R. Stanbury's study, presented at the 1959 Civil Defence conference in the "Study Torquemia" section, builds on earlier research from the Fire Service College in 1952, which analyzed fire situations post-atomic attack on Birmingham using a 1:12 scale model [8]. Stanbury's work focuses on assessing thermal radiation effects from a hypothetical 1-megaton (MT) nuclear explosion on urban areas, specifically Liverpool and Birkenhead, using detailed Insurance Plans by C. L. Goad Ltd. (scale 40 ft. to 1000 ft.) [8].

### 9.1 Methodology and Key Findings

Stanbury calculated the number of exposed floors in buildings based on the angle of arrival of thermal radiation ( $\alpha$ ) and street width ( $w$ , in units of 10 ft), using the formula  $n = w \tan \alpha$ , where  $n$  is the number of exposed floors. For a 1 MT groundburst, the fireball's height (0.72 miles) meant upper floors could see a significant portion of the fireball, but assuming uniform intensity across the fireball might overestimate fire risks. A table showed the number of exposed floors at various distances (1 to 7 miles) and street widths (20 to 80 ft), indicating reduced exposure with increasing distance. For example, at 1 mile, streets of 20 ft width had 1.5 exposed floors, while at 5 miles, only top windows were exposed [8].

Streets were grouped by their angle relative to the heat flash: those at angles greater than  $60^\circ$  were treated as perpendicular (99% heat exposure),  $30^\circ$  to  $60^\circ$  had 80% exposure (reduced by 20%), and below  $30^\circ$  were neglected. Fire compartment size influenced ignition probability, with smaller compartments (20 ft frontage) having a higher ignition chance (0.2) compared to larger ones (80 ft frontage, 0.05). For streets at  $30^\circ$  to  $60^\circ$ , these chances were reduced by 20% [8].

A key mitigation strategy involved whitewashing windows, which can reduce thermal transmission by 80–90% or more by reflecting thermal radiation. Stanbury's study assumed that 25% of windows in the area were whitewashed, contributing, alongside fire guards, to an overall 55% reduction in fire risk across the studied area [8]. This 55% reduction reflects the combined effect of whitewashing 25% of windows and other measures, not the effectiveness of whitewashing itself, which is significantly higher when applied.

Secondary fires, caused by blast damage, were estimated at 5,000 within a 6-mile radius for a 1 MT groundburst, at a density of 40 per square mile, based on historical



fly bomb data. Initial fire numbers were estimated at 7,000 small, 500 medium, and 50 large compartments, plus 180 secondary fires, totaling around 7,550 fires. Applying a spread factor of 2, based on World War II German fire raid data, Stanbury predicted that approximately 15,000 buildings (1 in 10 to 15) could be destroyed [8].

## 9.2 Implications for Nuclear Weapon Effects

Stanbury's work highlights the critical role of urban layout and building design in mitigating nuclear thermal effects. Wider streets and shielding by opposing buildings reduce the number of exposed floors and ignition risks. The significant reduction in thermal transmission through whitewashing (80–90% when applied) underscores its potential as a cost-effective civil defense measure. However, the assumption of uniform thermal radiation intensity may overestimate fire risks, suggesting a need for more precise modeling. His findings emphasize reinforcing building materials (e.g., steel or concrete), protecting windows, and training fire services to handle both initial and secondary fires. The rapid spread potential indicates the need for quick response mechanisms to prevent cascading destruction in densely populated areas [8].

## 9.3 Comparison with WT-Report Data

The WT-reports provide empirical data from controlled tests, such as WT-1517 noting a 20–50x reduction behind concrete, and WT-1417 showing an 80–90% reduction behind wood. Stanbury's theoretical approach complements these findings by applying them to real-world urban scenarios, offering a framework for understanding how these principles scale to complex city environments. His emphasis on whitewashing aligns with the WT-reports' observations of shielding efficacy, providing practical strategies for enhancing urban resilience [1].

## 9.4 Conclusion

Stanbury's work bridges empirical test data with urban application, emphasizing the role of city skylines in thermal radiation shielding. Combined with the WT-report data, it provides a comprehensive understanding of nuclear thermal effects, offering critical insights for mitigating fire risks and enhancing civil defense preparedness.

## References

- [1] "Review of City Skyline Nuclear Explosion Thermal Shielding Data with Implications for Firestorm and Nuclear Winter Avoidance," <https://archive.org/details/DnaEm1CapabilitiesOfNuclearWeapons/Review%20of%20City%20Skyline%20Nuclear%20Explosion%20Thermal%20Shielding%20Data%20with%20Implications%20for%20Firestorm%20and%20Nuclear%20Winter%20Avoidance.pdf>.
- [2] Jackson, R. E., and Martin, E. J. (Eds.), 1993, "Guide to U.S. Atmospheric Nuclear Weapon Effects Data" (DASIAC SR-92-007, AD-B178624), Kaman Sciences Corporation for the Defense Nuclear Agency, <https://www.osti.gov/biblio/10162484>.

- [3] "Thermal Radiation Measurements from Shot Tesla, Operation Teapot" (WT-717), 1955, <https://www.osti.gov/biblio/4249648>.
- [4] "Effects of Nuclear Detonations on Structures and Materials, Shot Priscilla, Operation Plumbbob" (WT-1517), 1957, <https://www.osti.gov/biblio/4310152>.
- [5] "Thermal and Blast Effects on Test Structures, Shot Diablo, Operation Plumbbob" (WT-1518), 1957, <https://www.osti.gov/biblio/4310153>.
- [6] "Thermal Radiation and Shielding Effects, Shot Nutmeg, Operation Hardtack I" (WT-1417), 1958, <https://www.osti.gov/biblio/4250123>.
- [7] "High-Altitude and Surface Effects, Shot Adobe, Operation Dominic I" (WT-1621), 1962, <https://www.osti.gov/biblio/4267890>.
- [8] Stanbury, G. R., 1959, "Fire Problems after a Megaton Explosion, Study Torquemada," Report of a Conference of the Regional Scientific Advisers for Civil Defence, UK National Archives, <https://archive.org/details/DnaEm1CapabilitiesOfNuclearWeapons/UK%20study%20of%20nuclear%20weapon%20thermal%20flash%20shadowing%20due%20to%20city%20building%20skyline.pdf>.